

Chapter 24

MRA and Flow quantification

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- **Previous classes**

- Flow and flow compensation (Chap. 23)
- Steady state signal (Cha. 18)

- **Today's content**

- MRA techniques
- Phase contrast flow quantification (PC FQ)

MR Angiography

- Bright blood methods
 - Time-of-flight (TOF)
 - Contrast enhanced MRA (CE MRA, Gd based)
 - SSFP (T2/T1 weighted)
- Dark blood methods
 - Double inversion recovery (DIR)
 - Flow dephasing
 - Saturation band
 - SWI (for veins)
 - Contrast enhanced (iron based USPIO)
- Quantitative
 - PC Flow quantification (FQ)
 - 4D FQ

Time-of-flight (TOF)

- Inflow & outflow effect
 - Critical speed: $v_c \equiv TH/T_R$
 - Inflow: unexcited/unsaturated blood
 - Outflow: excited blood

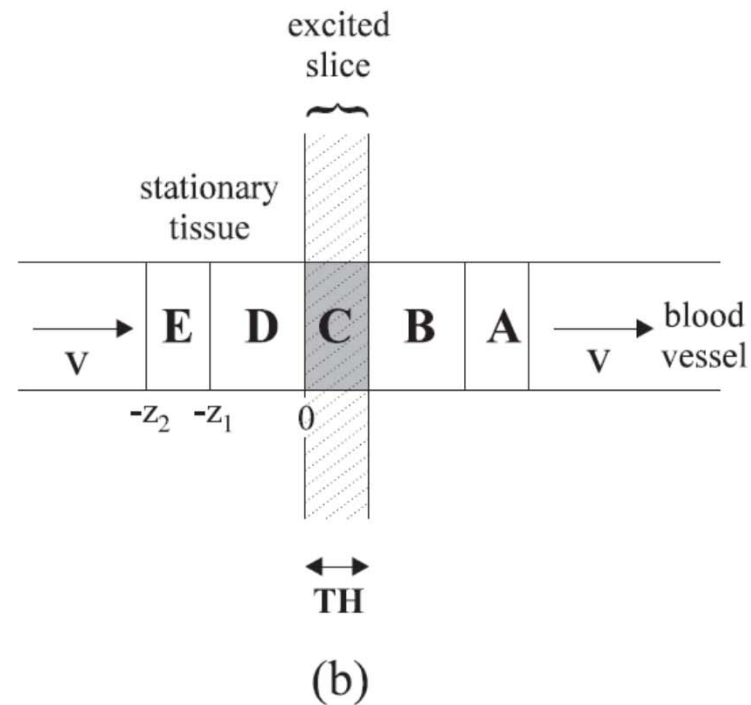
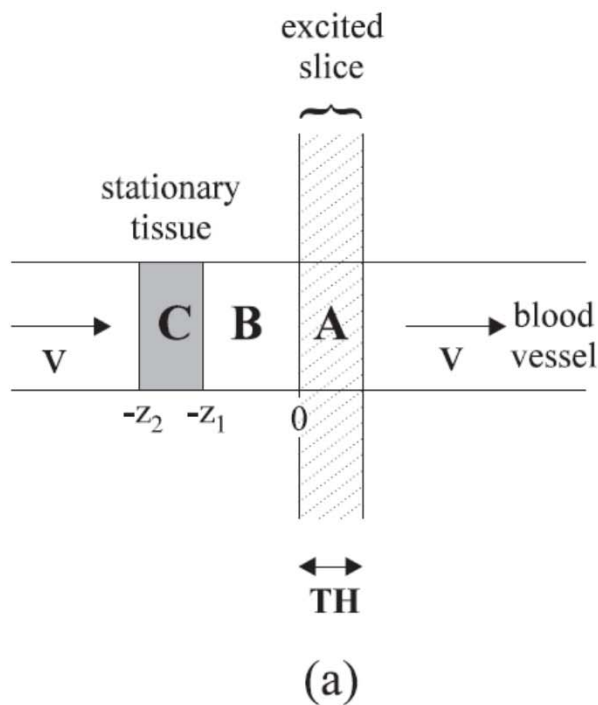
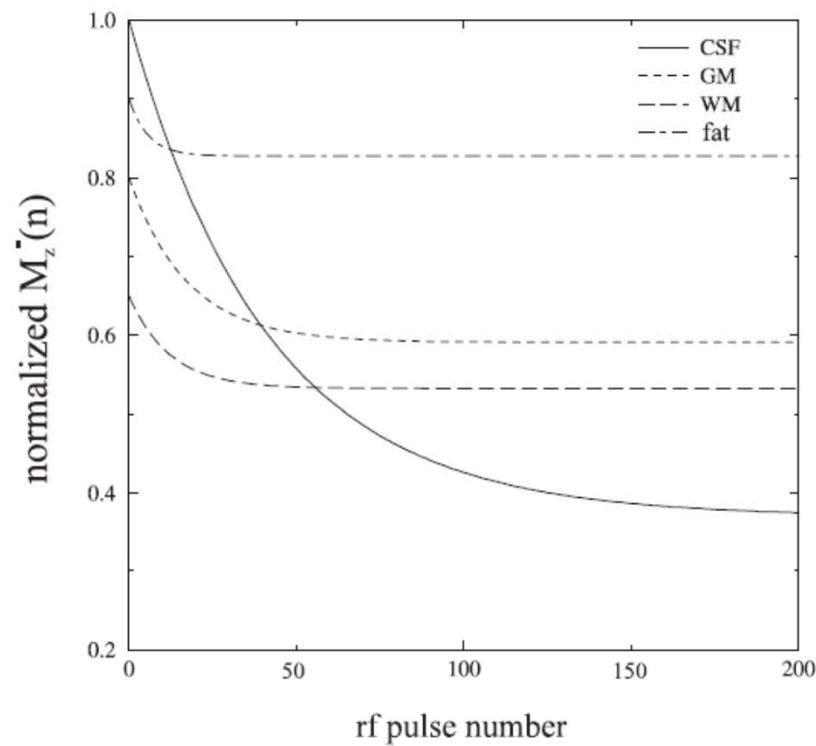


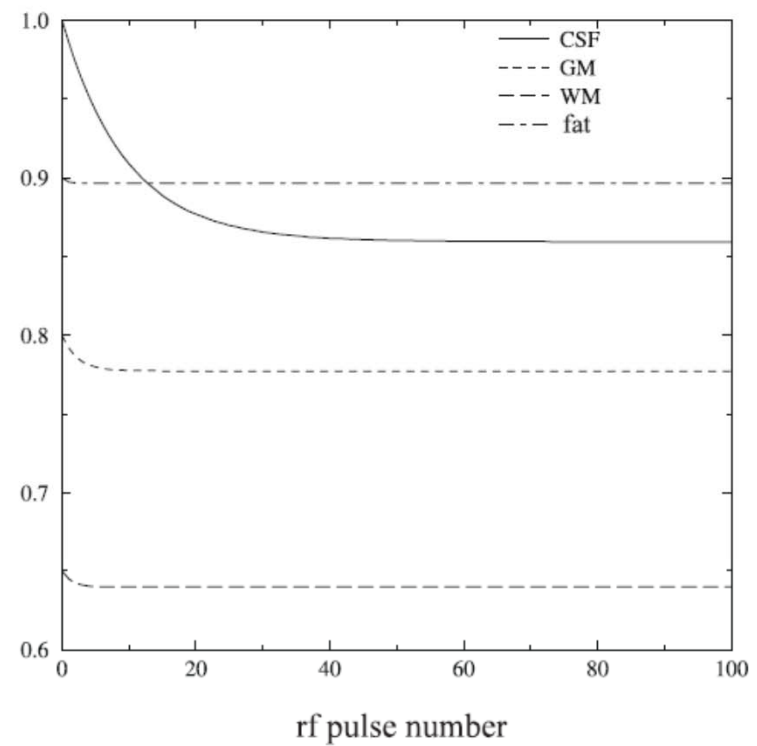
Fig. 24.1

Time-of-flight (TOF)

- SSI signal built-up: revisit



(a)
 $TR=40\text{ms}$



(b)
 $TR=400\text{ms}$

Fig. 18.5

Time-of-flight (TOF)

- Inflow saturation effect (2D)

$$\begin{aligned}
 S(p \geq n) &= \Lambda \frac{\sin \theta}{n} \sum_{m=1}^n \left(M_{ze} + (M_0 - M_{ze}) q^{m-1} \right) \\
 &= \Lambda \sin \theta \left(M_{ze} + (M_0 - M_{ze}) \frac{1 - q^n}{n(1 - q)} \right)
 \end{aligned}$$

n is maximal RF number the blood sees while in the slice
 $q \equiv E1 \cos \theta$

Therefore, for a thin 2D slice (relative to the flow velocity), very high signal can be obtained for vessels, while tissues are T_1 saturated

$$T_{1,flow} \equiv \frac{TH}{v} \quad \rightarrow \quad \frac{1}{T_{1,eff}} = \frac{1}{T_1} + \frac{1}{T_{1,flow}}$$

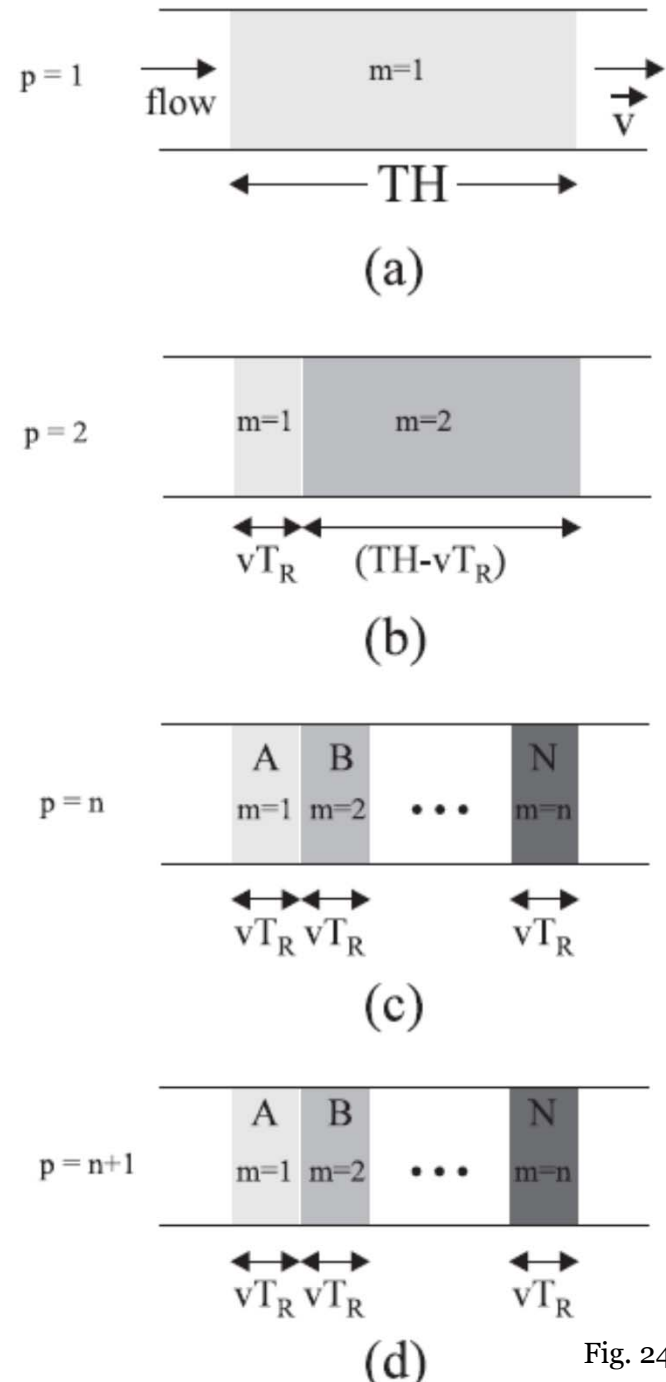
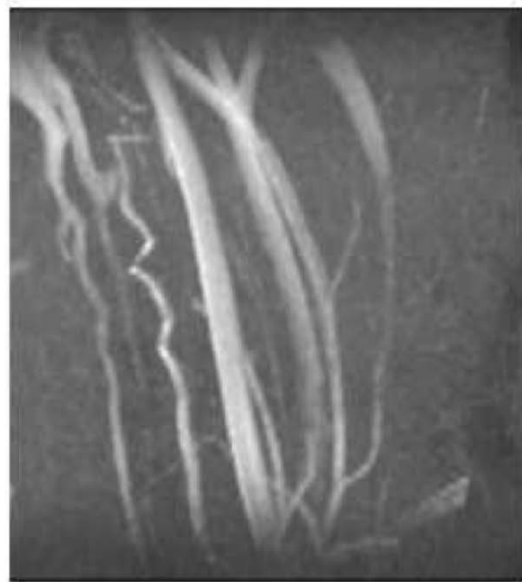


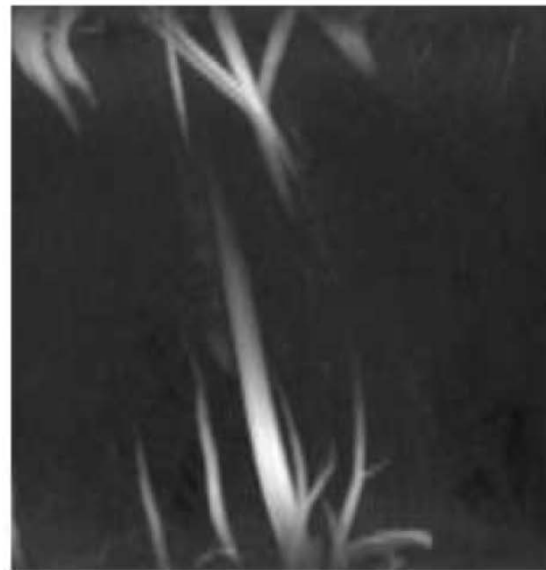
Fig. 24.3

Time-of-flight (TOF)

- Inflow saturation effect (3D)

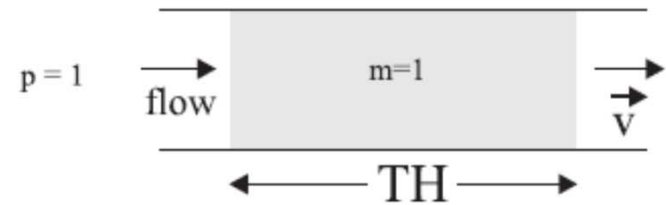


(a)

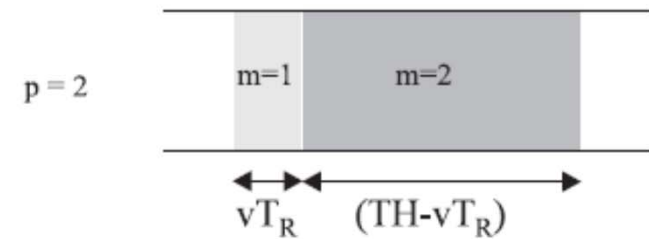


(b)

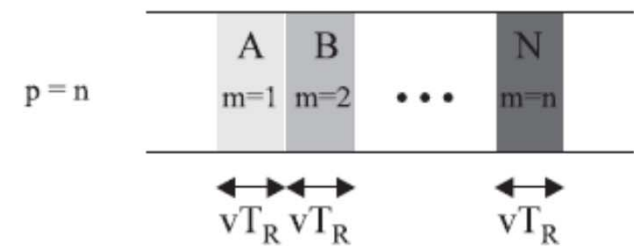
Fig. 24.6



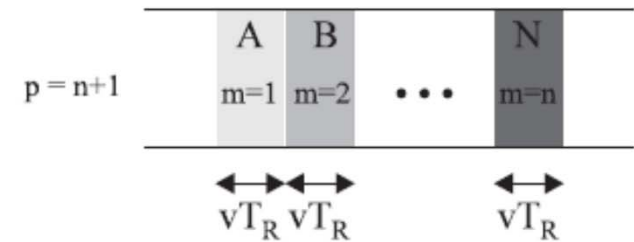
(a)



(b)



(c)



(d)

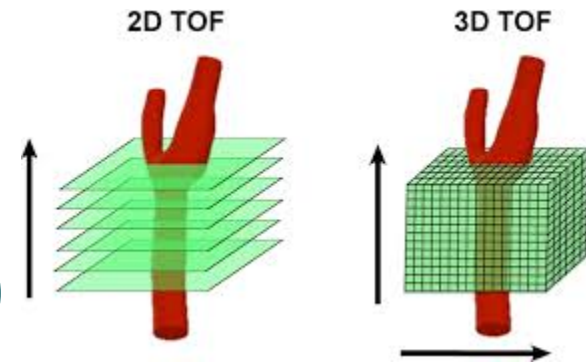
Fig. 24.3

Time-of-flight (TOF)

- TOF MRA has low tissue signal at steady state (saturated), but high inflow blood signal before steady state (unsaturated)
- Sequence and imaging consideration
 - Flow compensation
 - Perpendicular inflow
 - Multiple thin slabs
 - Short TE, short TR, properly small flip angle
 - TONE pulse (3D): spatially varying flip angle along slab thickness

Time-of-flight (TOF)

- 3D vs. 2D
 - SNR or resolution (esp. slice sel)
 - Blood saturation effect (or CNR)
 - TONE pulse
 - Vessel contours
 - Imaging time
 - Application dependent
 - Multiple slice / slab imaging
 - Arteries and veins



CE-MRA

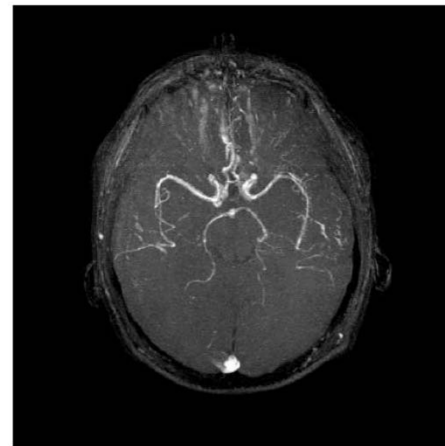
- SSI signal

$$SSI = \frac{M_0(1 - E1)}{(1 - E1\cos\theta)} \sin\theta E2$$

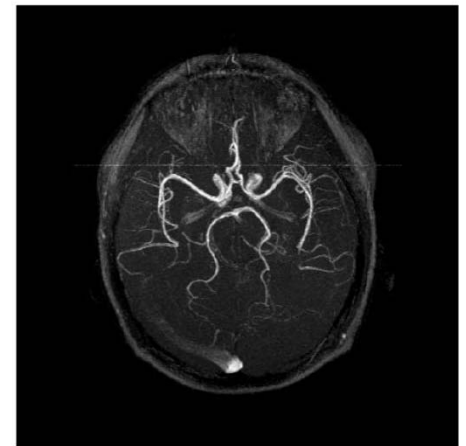
- To increase SSI signal (theoretically)
 - Short TE
 - Long TR
 - Ernst angle
 - Reduce T1 or increase T2

CE-MRA

- Use T1 shortening contrast agent (Gadolinium based chelates, or Gd) to reduce blood T1
- Flow independent, i.e. non TOF effects
- Consideration
 - Dosage: safety, T1 shortening effects
 - Shorter TR and higher flip angle can be used than TOF
 - Faster scans, or higher resolution
 - No TONE pulse needed
 - Venous signal



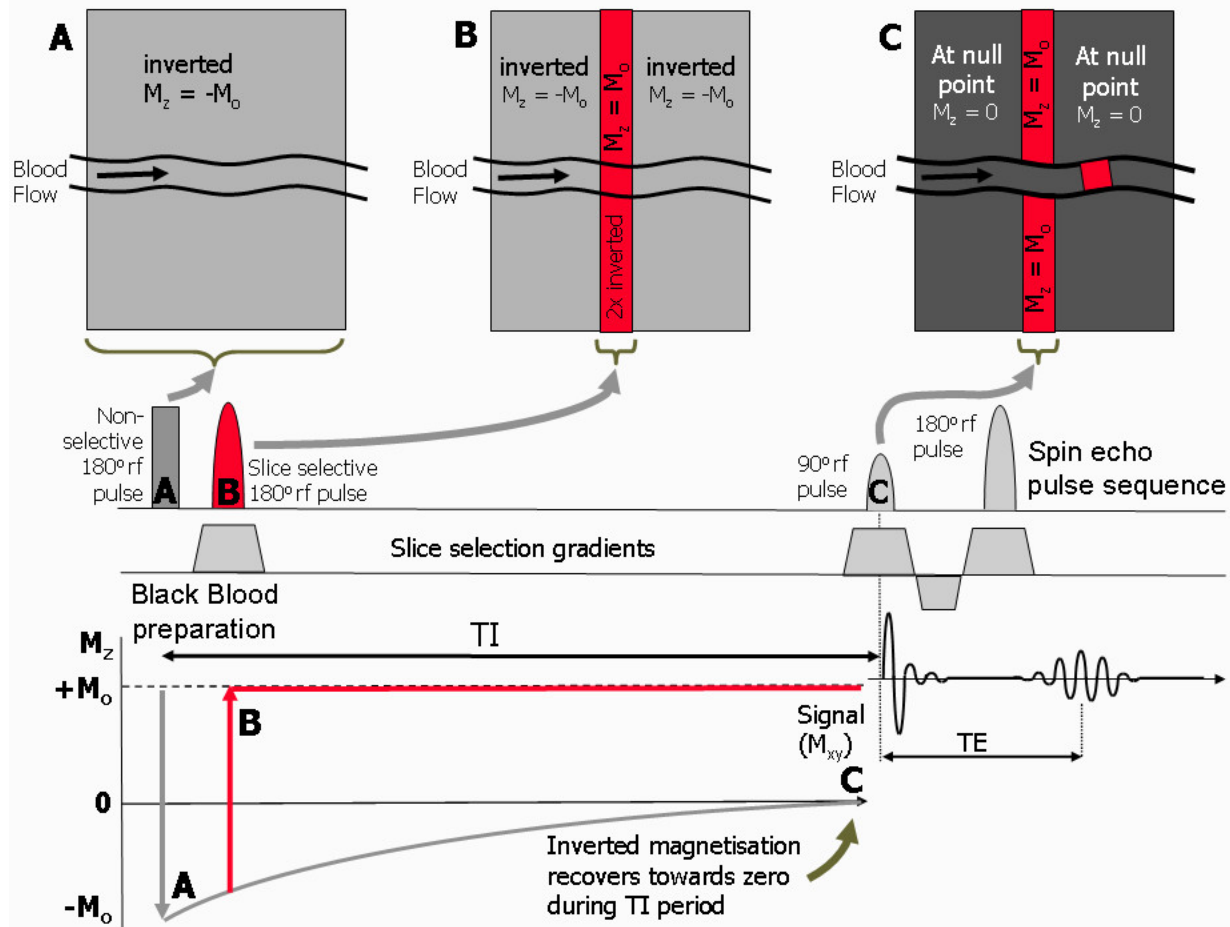
(a)



(b)

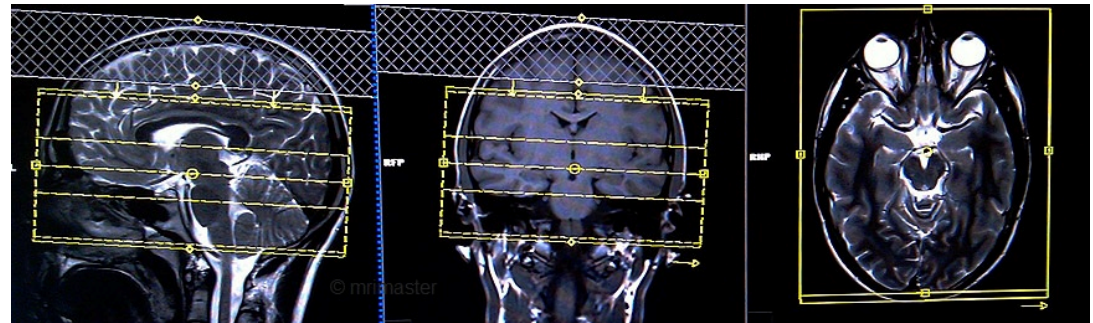
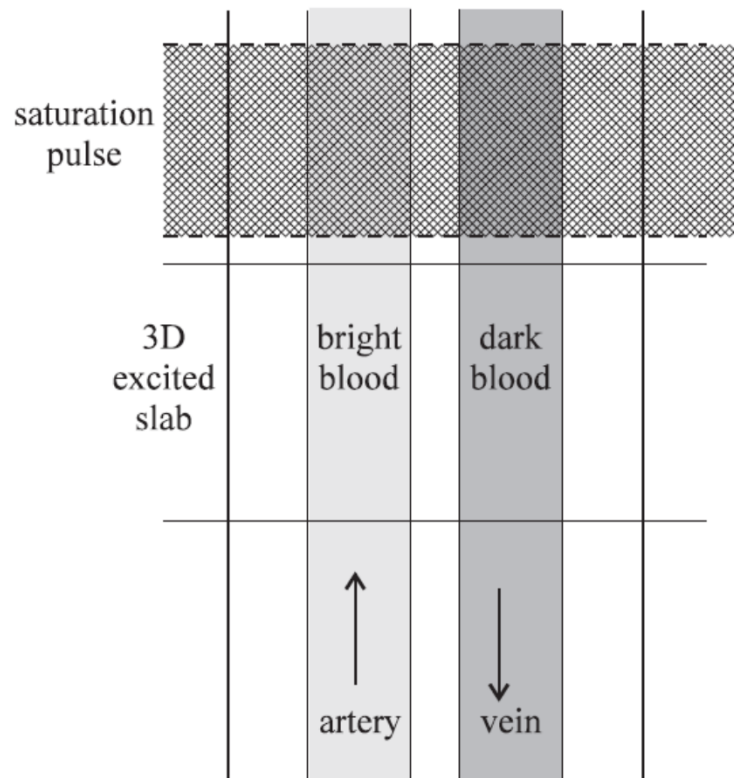
Black blood MRA

- Suppress inflow signal using DIR

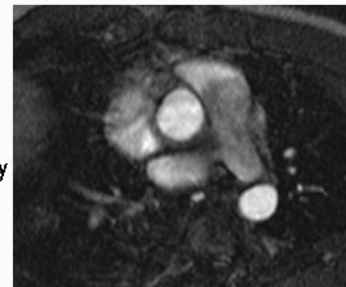
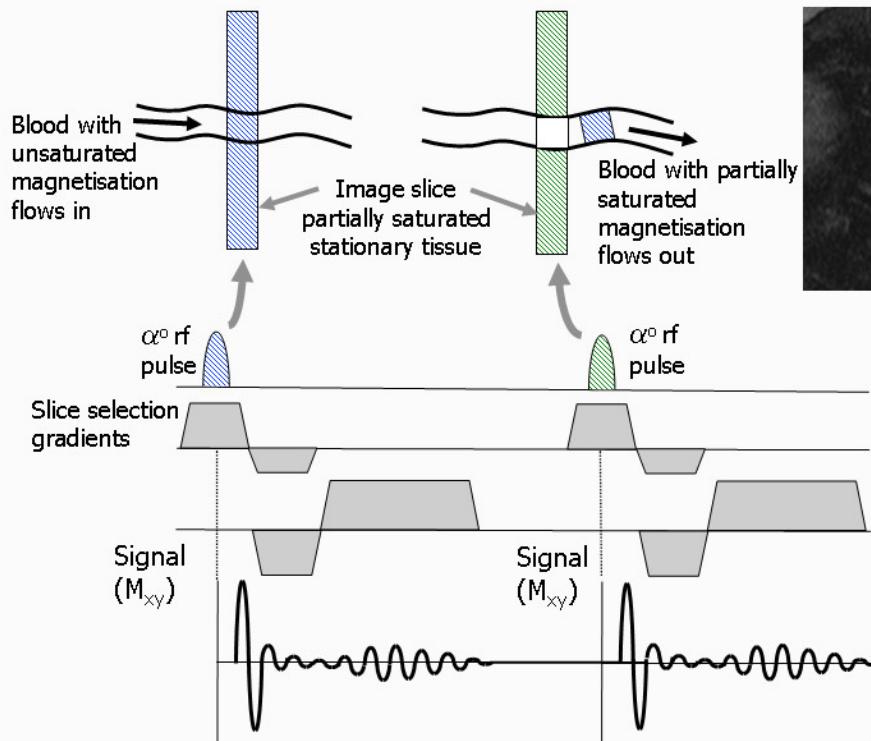


Black blood MRA

- Suppress inflow signal using Saturation band



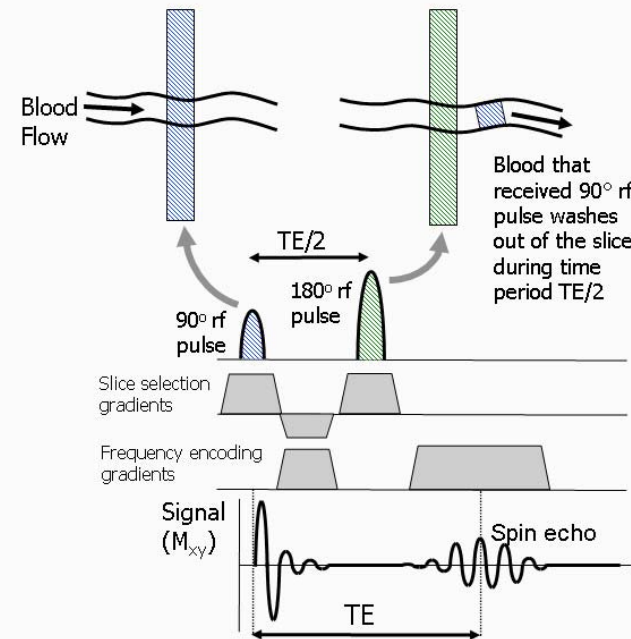
Black blood MRA



'Bright blood' spoiled gradient echo image

- Increased inflow signal using gradient echo

- Suppress inflow signal using Spin Echo



'Black blood' spin echo image

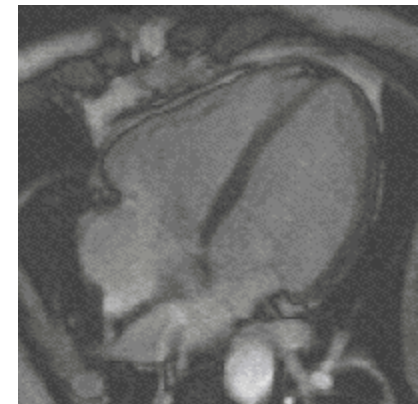
SSFP MRA

- $TR \ll T_2, T_1$

$$M_y^+(\infty) = \frac{M_0(1 - E_1) \sin \theta}{(1 - E_1 \cos \theta) - E_2(E_1 - \cos \theta)}$$

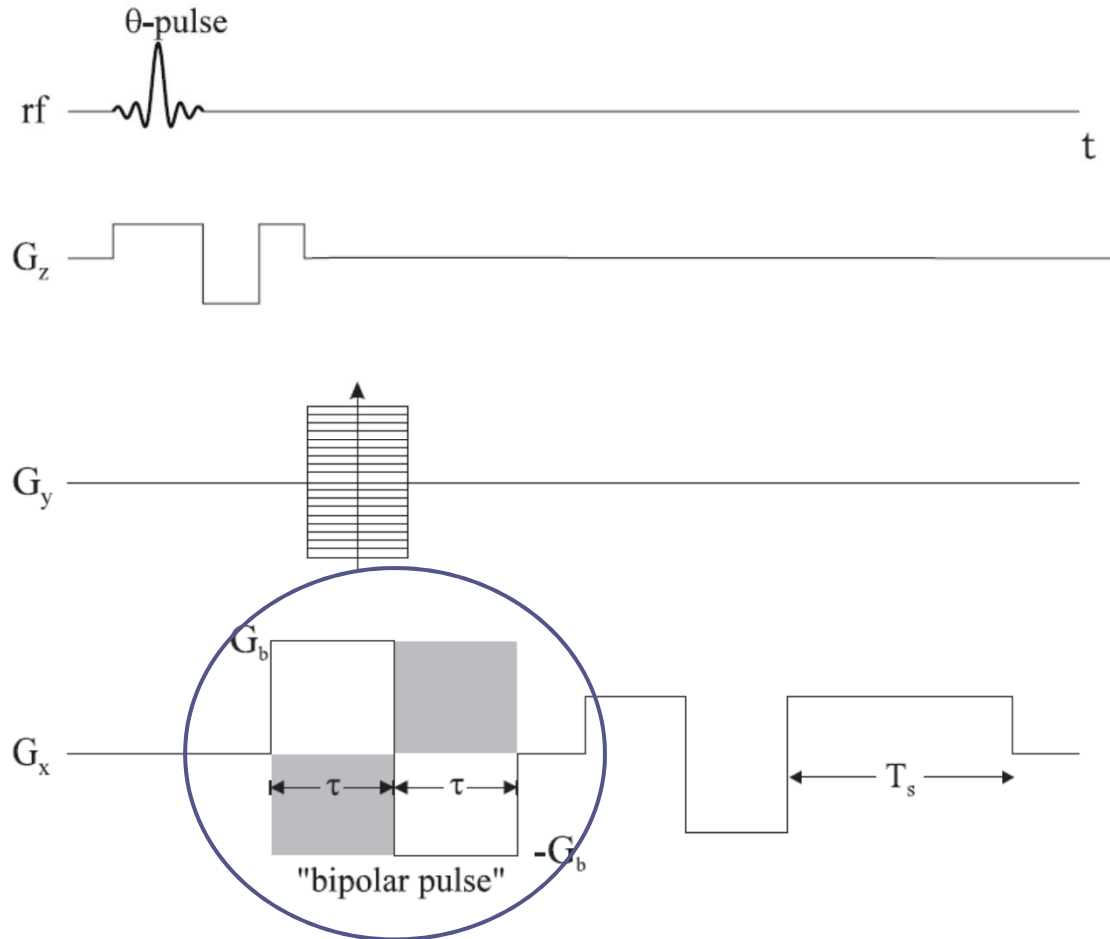
$$\approx \frac{M_0 \sin \theta}{\left(\frac{T_1}{T_2} + 1\right) - \cos \theta \left(\frac{T_1}{T_2} - 1\right)}$$

$$M_y^+(\infty)|_{\theta=\theta_{opt}} \simeq \frac{1}{2} M_0 \sqrt{\frac{T_2}{T_1}}$$



CSF and blood have high
 T_2/T_1 ratio:
Flow independent MRA

Phase contrast



VENC: velocity encoding
or

$$\text{VENC value} = \pi/(\gamma G \tau^2)$$

Why bipolar gradient?

Why flow compensation
after flow encoding?

$$\phi_v(t) = -\gamma \int G(\tau) v \tau d\tau \quad \longrightarrow \quad \phi_{v\pm} \equiv \phi_{v_x}(T_E) = \mp \gamma G v_x \tau^2$$

Phase contrast

$$\phi_{v\pm} \equiv \phi_{v_x}(T_E) = \mp \gamma G v_x \tau^2$$

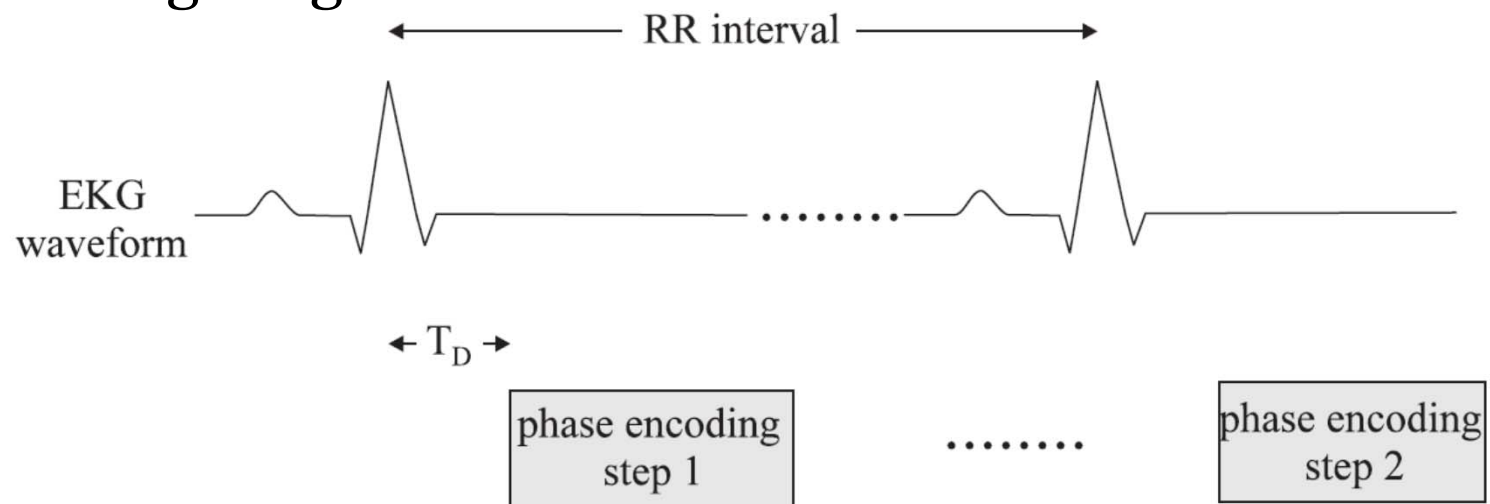
- Error source
 - Field inhomogeneity lead to phase variation
 - RF penetration effects (B1 field inhomogeneity)
 - Unknown phase baseline
 - Phase aliasing due to fast flow + low VENC
 - Low phase CNR due to slow flow + high VENC
- Solutions
 - Subtraction on phase images or complex division between two image sets with opposite VENC values
 - Set VENC value according to $\pi/(\gamma G \tau^2)$ to avoid aliasing

Flow quantification

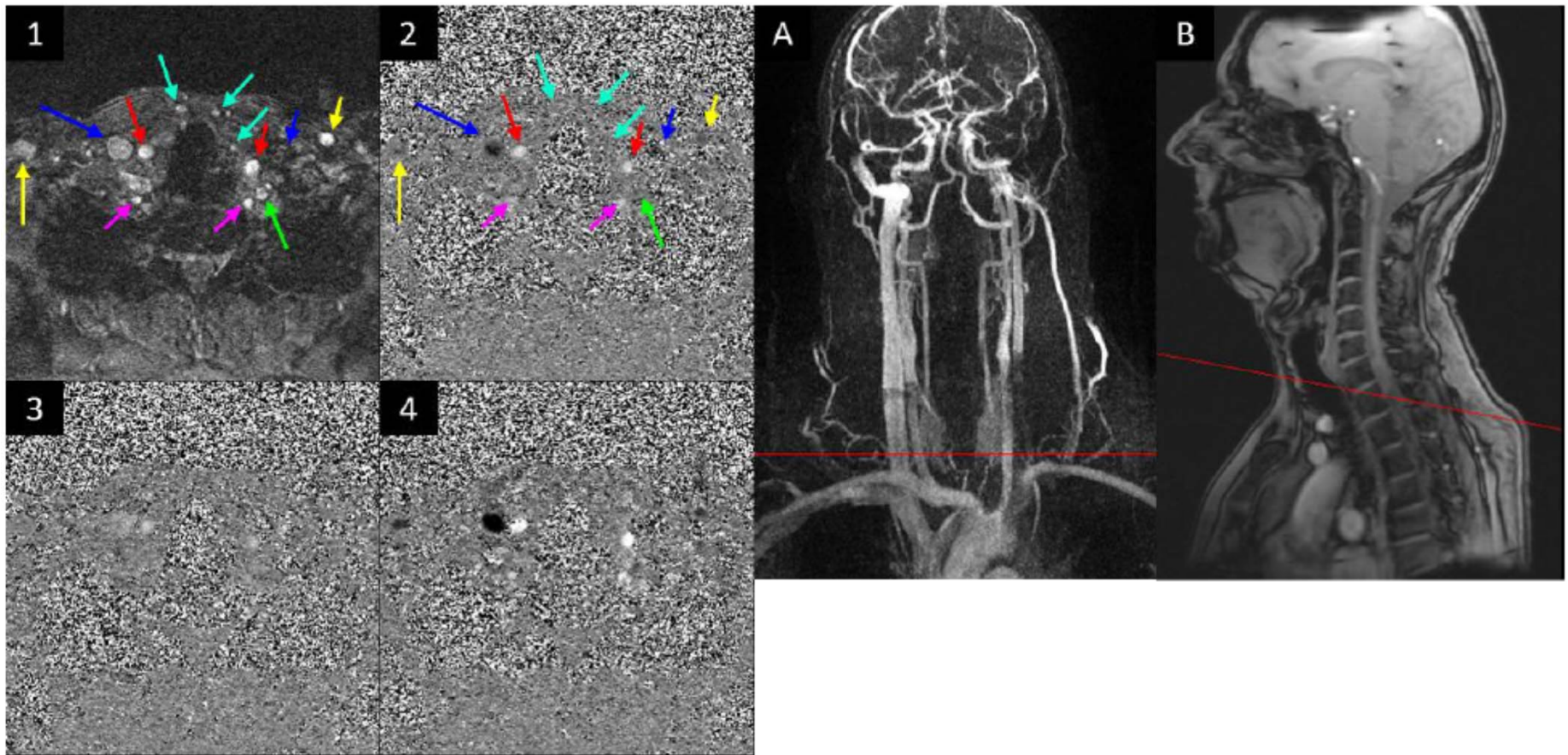
- Definition

$$F = \int v_z dA$$

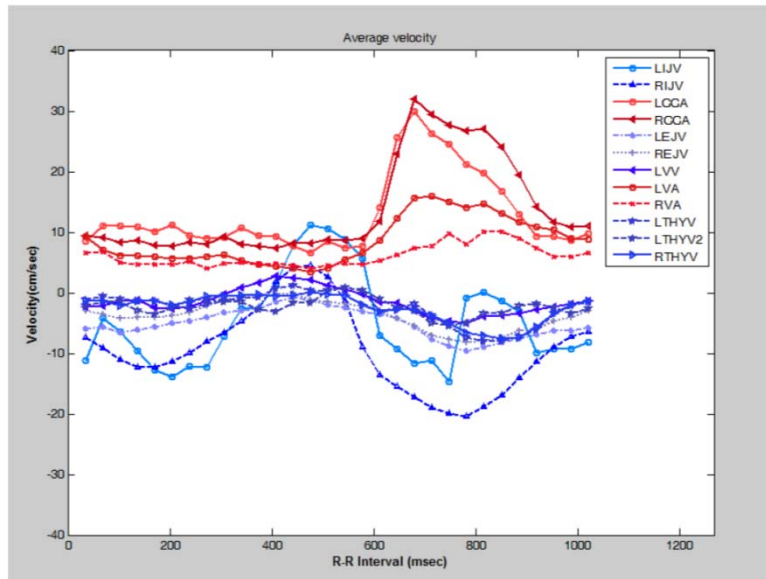
- Practically, flow refers to the blood volume that passes through a vessel in a give duration such as a cardiac cycle
- Cardiac gating



Flow quantification

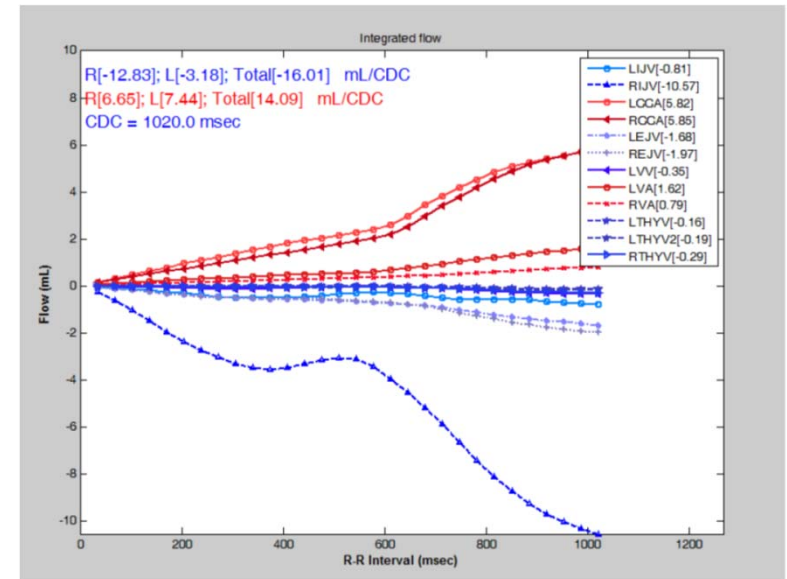


Flow quantification

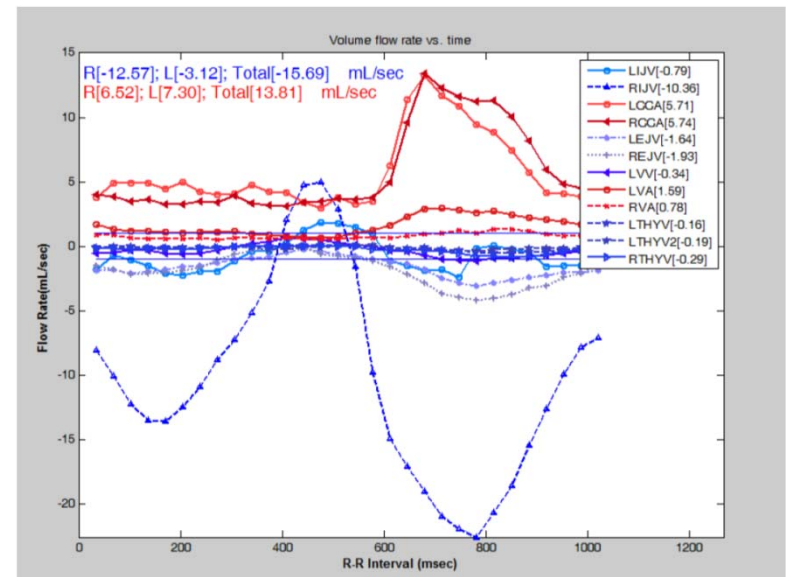


Average flow (cm/s)

Example:
Reflux flow in Right Internal Jugular Vein



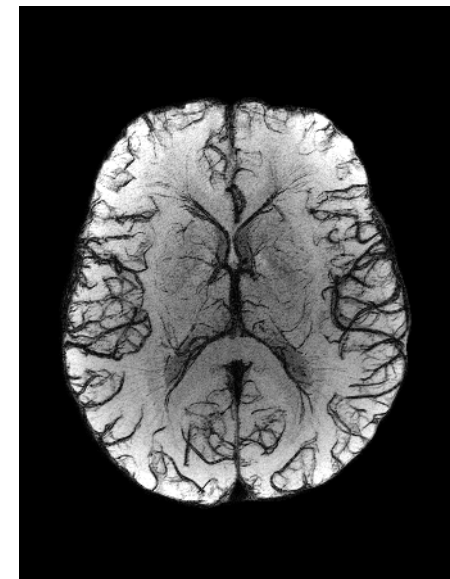
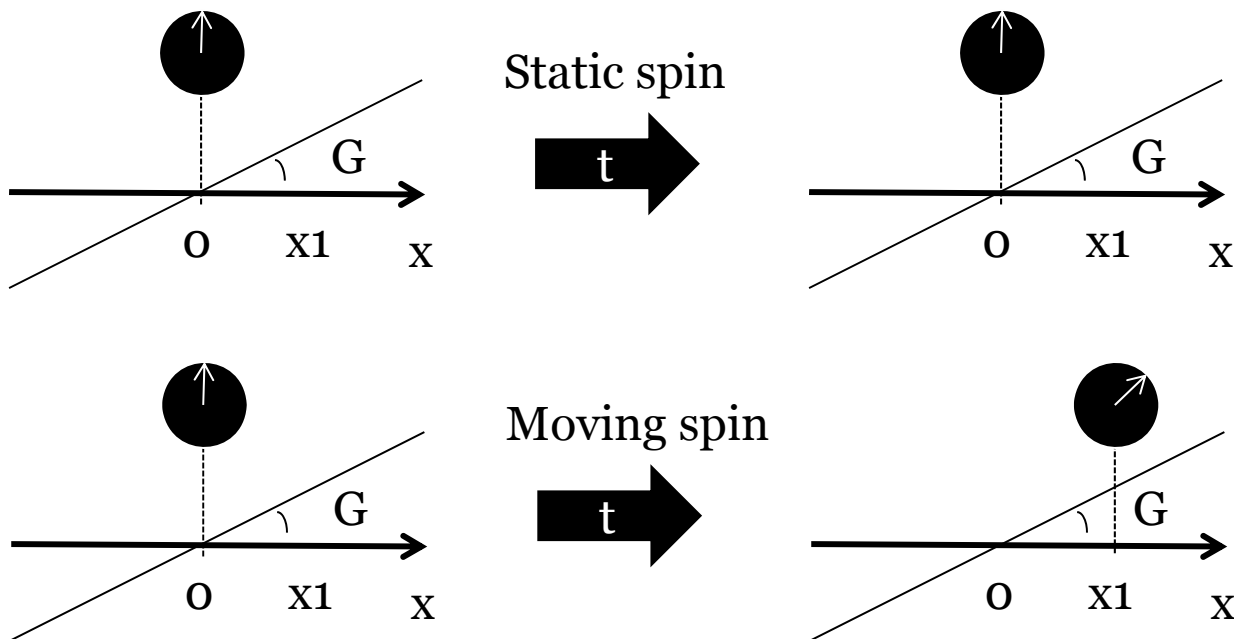
Integrated flow (ml)



Volume flow rate (ml/s)

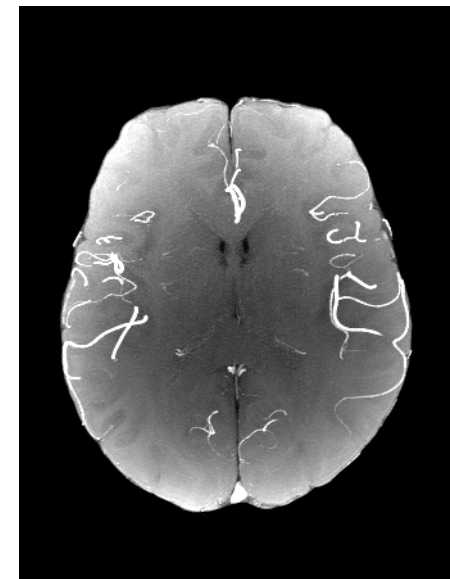
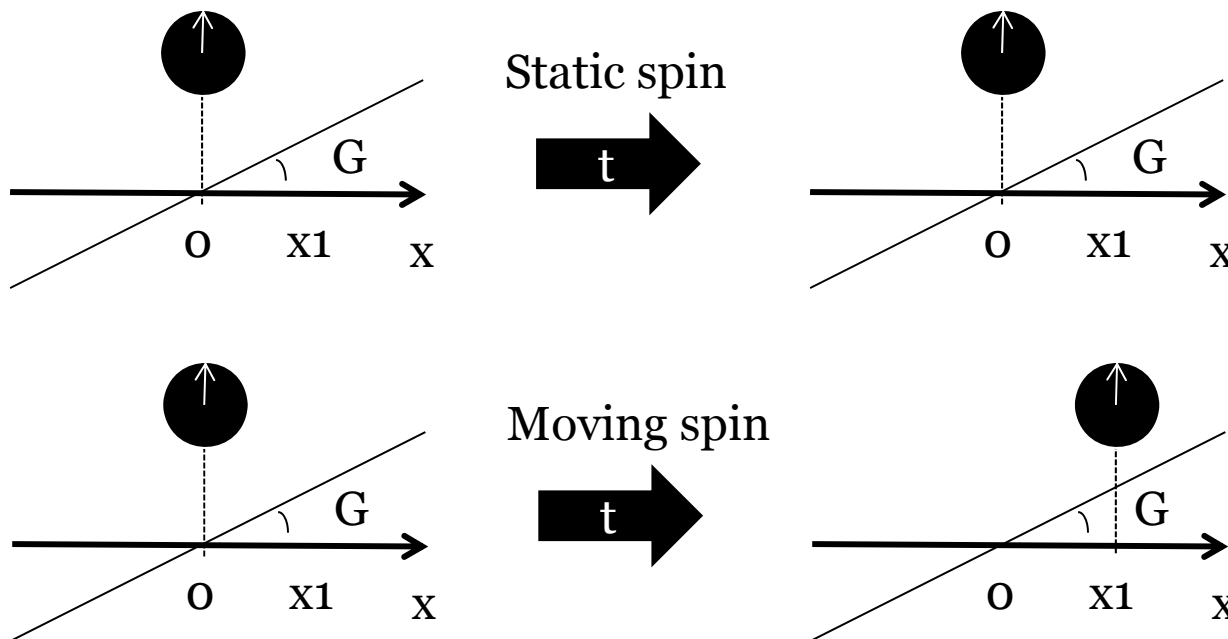
Imaging examples

- Flow related contrast (Macroscopic)
 - Flow dephasing (BG/bipolar dephasing gradient)
 - Flow compensation
 - Flow encoding



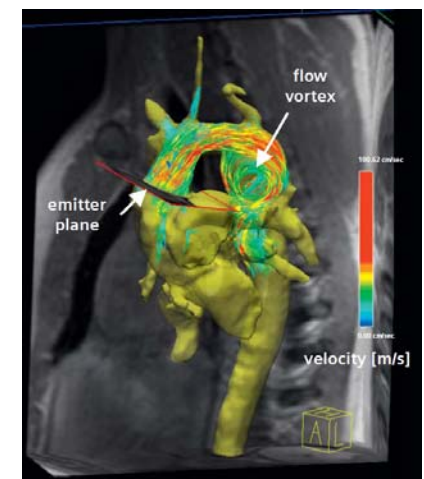
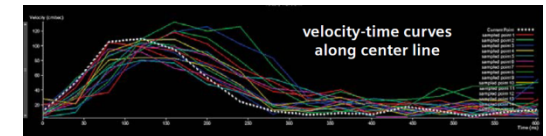
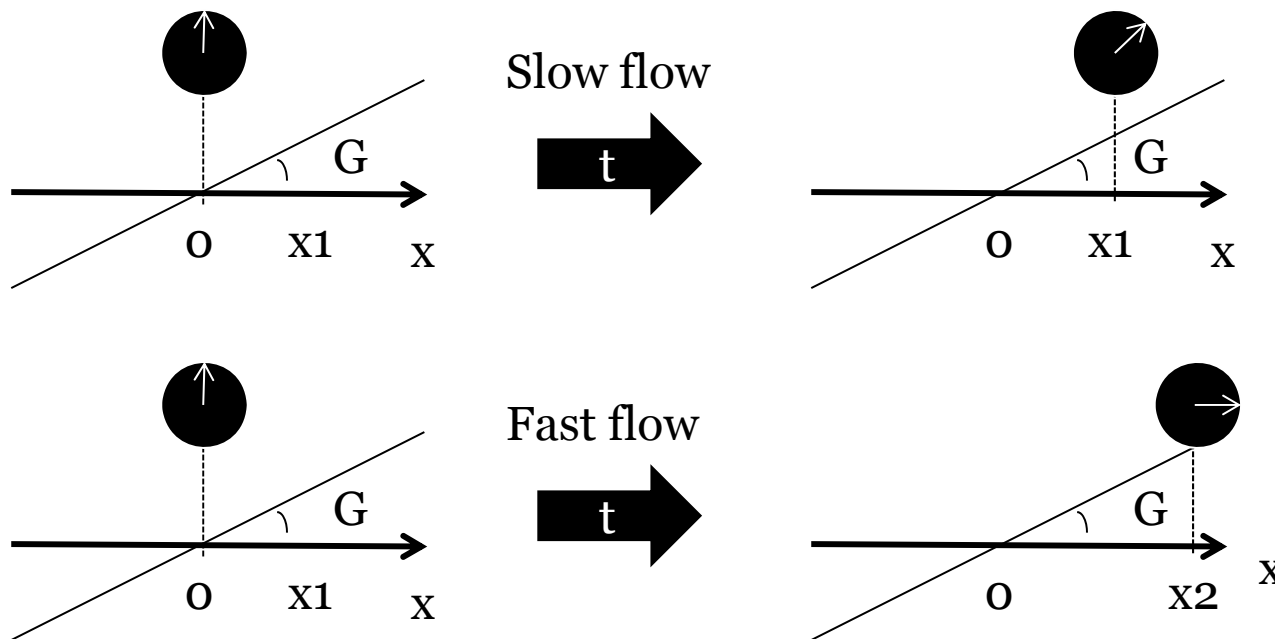
Imaging examples

- Flow related contrast
 - Flow dephasing
 - **Flow compensation (1st moment nulling gradient)**
 - Flow encoding



Imaging examples

- Flow related contrast
 - Flow dephasing
 - Flow compensation
 - Flow encoding (quantification)



4D flow, Michael Markl



Homework

- *Prob 24.2, 24.3, 24.4, 24.12, 24.18*

Next Session

Review & discussion

Ready to hand in your presentation essay